

**R-C phase shift oscillator:** The phase shift network consists of three sections  $R_1C_1$ ,  $R_2C_2$  and  $R_3C_3$ . To introduce a phase change of  $180^\circ$ . This phase shift of  $180^\circ$  is obtained with three sections  $C_1R_1$ ,  $C_2R_2$ ,  $C_3R_3$  (each section consists of a series coupling capacitor and a shunt resistor) each shifting the signal by  $60^\circ$ . The phase shift comes about because R and C provides a current which leads the applied voltage by certain angle. The smaller is the capacitance more will be current lead the voltage for a given resistance. with a proper choice of R and C, a phase shift of  $60^\circ$  per section is achieved.

To problem of a phase shift network for a transistor is some what complicated in comparison to vacuum tube because of low input impedance of the transistor. The last resistance in RC combination is not simply  $R_3$  but the transistor input resistance is parallel with  $R_3$ .

Now the frequency determining resistors are equal and similarly the frequency determining capacitors are equal i.e.

$$R_1 = R_2 = R_3 = R \text{ (say)}$$

$$\text{and } C_1 = C_2 = C_3 = C \text{ (say)}$$

Consider the frequency of oscillation and attenuation of the network, we proceed as follows, Fig(2) shows the equivalent circuit in which  $I_1$  is the signal current from the oscillator circuit and  $I_2$  is the signal current into the base circuit.

Applying Kirchoff's Law, we have

$$I_1 R = I_2 \left( 2R - \frac{j}{\omega C} \right) - I_3 R \quad (1)$$

$$I_2 R = I_3 \left( 2R - \frac{j}{\omega C} \right) - I_4 R \quad (2)$$

Eliminating  $I_2$  from eqn (1) and (2) & substituting the value of  $I_2$  from eqn (2) into eqn (1) we have

$$I_1 R = \left\{ \frac{I_3 \left( 2R - \frac{j}{\omega C} \right)}{R} - I_4 \right\} \left( 2R - \frac{j}{\omega C} \right) - I_3 R \quad (3)$$

$$\text{or } I_1 R = \frac{\left( 2R - \frac{j}{\omega C} \right)^2}{R} I_3 - \left( 2R - \frac{j}{\omega C} \right) I_4 - I_3 R \quad (4)$$

Substituting the value of  $I_3$  from eqn (3) in eqn (4), we get

$$I_1 R = \left\{ \frac{\left( 2R - \frac{j}{\omega C} \right)^2 \left( R - \frac{j}{\omega C} \right)}{R^2} \right\} I_4 - \left( 2R - \frac{j}{\omega C} \right) I_4 - I_4 \left( R - \frac{j}{\omega C} \right)$$

$$\begin{aligned} \therefore \frac{I_1}{I_4} &= \frac{R^3}{\left( 2R - \frac{j}{\omega C} \right)^2 \left( R - \frac{j}{\omega C} \right) - \left( 3R - \frac{2j}{\omega C} \right) R^2} \\ &= \frac{R^3}{R^3 - j \frac{6R^2}{\omega C} - \frac{5R}{\omega^2 C^2} + \frac{j}{\omega^3 C^3}} \quad (5) \end{aligned}$$

For a phase shift of  $180^\circ$  between  $I_4$  and  $I_1$ , the terms containing  $j$  should vanish and we have

$$\frac{j}{\omega^3 C^3} - \frac{j 6R^2}{\omega C} = 0$$

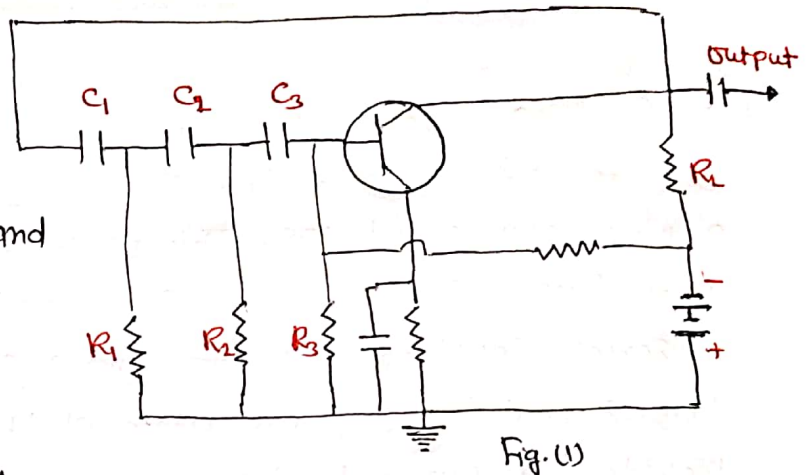


Fig. (1)

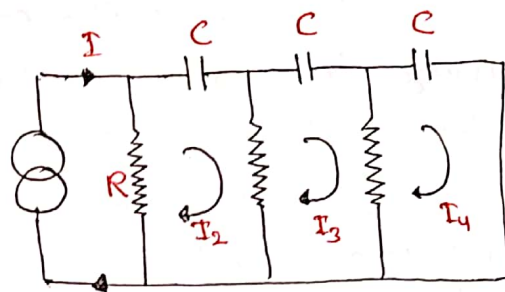


Fig. (2)

$$\text{or } \frac{1}{\omega^2 C^2} = GR^2$$

$$\therefore \omega = \frac{1}{\sqrt{G} \cdot RC} \quad \text{--- (6)}$$

The frequency of oscillations is given by

$$f = \frac{1}{2\pi\sqrt{G} \cdot RC}$$

At this frequency, from eqn (5), we have

$$\frac{I_4}{I_1} = \frac{R^3}{R^3 - \frac{SR}{C^2} \times GR^2 C^2} = -\frac{1}{29} \quad \text{--- (7)}$$

From eqn (7) it is clear that transistor must give a current gain of at least 29 to achieve oscillations. This is a transistor with high value of feed back is selected to give oscillations. For sinusoidal output the transistor must not oscillate too strongly and the gain should be adjusted to give only a small amplitudes of oscillations.

Teacher's Signature: \_\_\_\_\_